SUPPRESSION OF POWERLINE INTERFERENCE IN ECG USING ADAPTIVE DIGITAL FILTER

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Abstract
Artifacts in electrocardiogram (ECG) records are caused by various factors, such as powerline interference, electroencephalogram (EEG), electromyogram (EMG) and baseline wander. These noise sources increase the difficulty in analyzing the ECG and to obtaining clinical information. For that reason, it is necessary to design specific filters to decrease such artifacts in ECG records. In this paper, FIR adaptive filter based on a least mean square (LMS) algorithm for eliminating 50Hz powerline interference in ECG signal is proposed. The filter is designed with FDAtool of Matlab and tested with ECG signal corrupted with various powerline frequencies. Results are obtained and presented.

Keywords: Electrocardiogram, Matlab and Simulink, Least Mean Square (LMS) algorithm.

1. Introduction
ECG records carry information about abnormalities or responses to certain stimuli in the heart. Some of the characteristics of these signals are the frequency and morphology of their waves. These components are in the order of just a few up to 1mV and their frequency content within 0.5Hz and 100Hz depending on individual. The morphology and frequency are analyzed by physicians in order to detect heart disorders and heart related pathologies. However, the ECG signal is generally with other biological signals like electroencephalogram, electromyogram, baseline Wander and powerline interference. Due to the presence of artifacts, it is difficult to analyze the ECG, for they introduce spikes which can be confused with cardiological rhythms. Thus, noise and undesirable signals must be eliminated or attenuated from the ECG to ensure correct analysis and diagnosis.


2. Coefficient Update Process of Least Mean Square (LMS) Based FIR Adaptive Filter.
We can describe the FIR-LMS algorithm by considering the adaptive noise canceller(ANC) of fig 1 . There is a primary signal d(n) which in this case is the ECG signal plus powerline noise, and the secondary signal x(n)
which in this case is the powerline noise. The filter produces an output $y(n)$ which is subtracted from $d(n)$ to compute an error $e(n)$

$$e(n) = d(n) - y(n)$$ \hspace{1cm} (2)

\[ \therefore \text{substituting for } y(n) \text{ will give} \]

$$e(n) = d(n) - \sum_{k=0}^{L} h_k x(n-k)$$ \hspace{1cm} (3)

The Square Error is

$$e^2(n) = d^2(n) - 2d(n) \sum_{k=0}^{L} h_k x(n-k) + \left[ \sum_{k=0}^{L} h_k x(n-k) \right]^2$$ \hspace{1cm} (4)

The Square Error expectation for N samples is given by

$$E[e^2(n)] = \sum_{k=0}^{N} e^2(n)$$ \hspace{1cm} (5)
\[ E[e^2(n)] = \sum_{K=0}^{N} \left[ d^2(n) - 2d(n) \sum_{K=0}^{L} h_k \cdot x(n-k) + \sum_{K=0}^{L} h_k \cdot x(n-k) \right] \]

\[ = \sum_{n=1}^{N} \left[ d^2(n) - 2 \sum_{n=1}^{N} d(n) \sum_{K=0}^{L} h_k \cdot x(n-k) + \sum_{K=0}^{L} h_k \cdot x(n-k) \sum_{n=1}^{N} h_k \cdot x(n-k) \right] \]

\[ = \sum_{n=1}^{N} \left[ d^2(n) - 2 \sum_{n=1}^{N} h_k \cdot d(n) \cdot x(n-k) + \sum_{K=0}^{L} h_k \cdot h_l \cdot x(n-k) \cdot x(n-k) \right] \]

\[ E[e^2(n)] = \left[ d^2(n) - 2 \sum_{n=0}^{L} h_k \cdot R_{dx}(n) + \sum_{k=0}^{L} h_k \cdot h_l \cdot R_{xx}(n)(k-l) \right] \quad (6) \]

Where \( R_{dx}(n) \) is the cross-correlation function between the primary and secondary input signals while \( R_{xx}(n) \) is the autocorrelation function between the same two inputs. That is to say that

\[ R_{dx}(n) = \sum_{n=1}^{N} d(n) \cdot x(n-k) \quad (7) \]

\[ R_{xx}(n) = \sum_{n=1}^{N} x(n) \cdot x(n-k) \quad (8) \]

The objective of this update process is to minimize the squared error. To get this goal the optimization technique of steepest descent is used. With this it is possible to calculate the filter coefficient vector for each iteration \( k \), having information about the previous coefficients and gradient, multiplied by a constant. That is,

\[ h_k(n+1) = h_k(n) + \mu (\nabla_k) \quad (9) \]

Where \( \mu \) is a coefficient that controls the rate of update and it is called the step-size.

The gradient is defined as,

\[ \nabla_k = \frac{\partial e^2(n)}{\partial h_k(n)} \quad (10) \]

Using (10) in (9) yields

\[ h_k(n+1) = h_k(n) - \mu \frac{\partial e^2(n)}{\partial h_k(n)} \quad (11) \]

Differentiating with respect to \( h_k \) gives

\[ h_k(n+1) = h_k(n) - 2 \mu e(n) \frac{\partial e(n)}{\partial h_k(n)} \quad (12) \]

\[ h_k(n+1) = h_k(n) - 2 \mu e(n) \frac{\partial [d(n) - \sum_{k=0}^{L} h_k \cdot x(n-k)]}{\partial h_k(n)} \quad (13) \]

Since \( d(n) \) and \( x(n) \) are not functions of \( h_k \), (13) condenses to

\[ h_k(n+1) = h_k(n) - 2 \mu e(n) x(n-k) \quad (14) \]

The expression of (14) is the final description of the algorithm to compute the filter coefficients as a function of the signal error \( e(n) \) and the reference input signal \( x(n) \). The coefficient or step-size \( \mu \) is a scaler constant that must be chosen to guarantee fast convergence or adaptation without losing stability. The filter is stable if \( \mu \) satisfies the condition;

\[ 0 < \mu < \frac{1}{10LP_{xx}} \quad (15) \]
Where \( L \) is the order of the filter and \( P_{xx} \) is the power of the input signal computed as

\[
p_{xx} = \frac{1}{M+1} \sum_{n=0}^{M} x^2(n)
\]

The interpretation of (14) is that a new set of coefficients \( h_k(n+1) \) is generated by updating the previous coefficients \( h_k(n) \) in accordance with the reference input noise signal.

3 Design of FIR Adaptive noise canceller (ANC) using LMS Algorithm.
The canceller is for removing the 50Hz powerline interference. The order of the filter is 100 and the step size is 0.001. The design is carried out with FDAtool of Matlab. The instantaneous impulse, frequency and phase responses of the adaptive filter are depicted in fig. 12, fig. 13 and fig.14 respectively.

4 Results
Fig. 5 shows an ECG signal corrupt with 50Hz powerline while fig 6 depicts the frequency response. It can be seen from fig 6 that the power of the signal at 50Hz frequency is approximately (-45.21dB). Fig 7 shows the filtered ECG signal while fig. 8 is a representation of the frequency response. Fig 9 shows the estimated output of the adaptive filter. It is clear from fig 8 that the power of the filtered signal at 50Hz drops to (-58.19dB); which implies that the adaptive filter has removed the 50Hz powerline interference. Fig 7 is also a representation of a clean ECG and its comparison with fig 5 confirms removal of 50Hz powerline interference by the adaptive filter.
Fig. 5: ECG signal corrupt with 50Hz powerline

Fig. 6: Frequency response of ECG signal corrupt with 50Hz powerline

Fig. 7: ECG signal after filtration with the adaptive filter

Fig. 8: Frequency response of ECG signal after filtration with the adaptive filter
Fig. 9: Adaptive filter estimated output

Fig. 10 depicts an ECG signal corrupt, with 60Hz powerline interference and fig 11 is the frequency response. Fig 11 shows that the power of the signal at 60Hz is approximately (-46.12dB). Fig 12 shows the filtered signal and fig 14 is the frequency response. The estimated output signal is represented in fig 14. From fig 13 the power at 60Hz frequency drops to (-58.19dB), implying that the adaptive filter has removed the 60Hz noise. Comparing fig. 10 and fig 13 confirms noise removal.

Fig. 10: ECG signal corrupt with 60Hz powerline

Fig. 11: Frequency response of ECG signal corrupt with 60Hz powerline

Fig. 12: ECG signal after filtration with the adaptive filter
Fig. 13: Frequency response of ECG signal after filtration with the adaptive filter

Fig. 14: Estimated output of the adaptive filter

Fig. 15 shows an ECG signal corrupt with 45Hz powerline interference while fig. 16 is the frequency response.

From fig. 16 it can be seen that the power of the corrupt signal at 45 Hz is (-44.99dB ). When the corrupt signal is applied to the adaptive filter, the filtered output is shown in fig17 while the frequency response of the filtered output is shown in fig. 18. Fig. 19 is the estimated filter output. From fig 18, it can be confirmed that the power of the signal has reduced to (-57.78dB          ) which means that the adaptive filter has removed the 45Hz powerline. A comparison of fig. 16 and fig. 17 also provides the information that the adaptive filter has removed the 45Hz powerline noise.

Fig. 15: ECG signal corrupt with 45Hz powerline

Fig. 16: Frequency response of ECG signal corrupt with 45Hz powerline
5. Conclusion

The instantaneous impulse and magnitude responses of the adaptive filter show that the filter is very stable. The phase response is also indicating that the filter has a linear phase, which is desirable in filtering complex waves like ECG signal. The results of the implementation are confirming that when the frequency of the input noise changes, the adaptive filter tracks such changes and adjusts its coefficient to produce the same filtered output. Therefore, adaptive filter is most suitable when the frequency of the noise to be filtered out is not stable.

References


